PATENT SPECIFICATION

(54) CORROSION INHIBITING COMPOSITION

(71) We, CIBA-GEIGY AG., a Swiss Body Corporate, of Basle, Switzerland, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:—
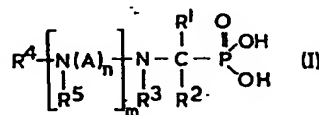
The present invention relates to a composition for inhibiting the corrosion of metal surfaces, particularly ferrous metals, in contact with aqueous systems.

In the past, water-soluble chromates and dichromates have been widely used for inhibiting the corrosion of metals in contact with aqueous systems. However, chromate and dichromate ions are toxic and pollute any stream or river into which water containing them is discharged and are therefore ecologically undesirable. Inorganic nitrites have been used as corrosion inhibitors, but it is usually necessary to use them at high dosage levels, often as much as 650 parts per million. Amino phosphonic acids have also been proposed as corrosion inhibitors, usually in conjunction with zinc or chromate ions or tannins since when used alone some amino phosphonic acids have the disadvantage that, being sequestering agents, they promote dissolution of the metal with formation of complexed ions.

A major advantage of inorganic nitrites is their cheapness, but this is offset by the fact that it is necessary to use them at high dosage levels. Clearly it would be most advantageous if a corrosion inhibitor combination could be devised, based on nitrite for cheapness, which had at least the same efficiency at much lower dose rates, that is if a suitable compromise could be reached between efficiency, dose rate and cost of use at that dose rate.

Surprisingly we have found that the combination of an inorganic nitrite and a member of certain classes of aminoalkyl phosphonic acids can result in a corrosion inhibitor which is better than could be foreseen from a knowledge of the properties of each, that is to say these compounds can form synergistic combinations. The mechanism of synergism is not simple; in chemical synergism, cases are well known of two or more materials which demonstrate significant synergy when combined in certain ranges of proportions; but whose combined effect is only additive (or even worse than additive) at other proportions, and this is the situation in the present case. All combinations we shall describe show synergism as we shall define it when combined in some proportions; in other proportions, the combined effect may merely be additive, or can be antagonistic.

According to this invention, there is provided a synergistic combination (as hereinafter defined) comprising a combination of an inorganic nitrite and a compound having the formula:

$$R^4 - \left[N(A)_n \begin{array}{c} | \\ R^5 \end{array} \right]_m N - \begin{array}{c} R^1 \\ | \\ C \\ | \\ R^3 \end{array} \begin{array}{c} \\ | \\ R^2 \end{array} \begin{array}{c} O \\ \| \\ P \end{array} \begin{array}{c} OH \\ \\ OH \end{array} \quad (I)$$

wherein R^1 and R^2 may be the same or different and each represents hydrogen or a hydrocarbyl or hydroxy-substituted hydrocarbyl radical each containing up to 8 carbon atoms, R^3 and R^4 may be the same or different and each represents hydrogen or a

hydrocarbyl or hydroxy-substituted hydrocarbyl radical each containing up to 8 carbon atoms, a carboxyalkyl or alkoxyalkyl radical each containing up to 3 carbon atoms, an alkylene phosphonic acid grouping containing up to 4 carbon atoms or an aralkylene phosphonic acid such that not more than two phosphonic acid groupings separated by less than two carbon atoms may be attached to any nitrogen atom, R^5 is hydrogen or an alkylene phosphonic acid containing up to 4 carbon atoms, A is a saturated divalent hydrocarbyl radical containing up to 6 carbon atoms, m is 0 or an integer from 1 to 60, n is 0 or 1; when m is 0, R^4 may be a hydroxy grouping or R^3 and R^4 together with the nitrogen atom may form a six membered ring, when m is 1, the grouping R^3N—A—NR^5 may form a heterocyclic ring, and when m is greater than 1, the constituent R^5 groupings may be the same or different; and the water-soluble salts thereof.

If desired, the radicals R^1, R^2, R^3, R^4 and R^5 of the compound of formula I may contain substituents which do not increase the water solubility or react in aqueous solutions, for example, chlorine.

The water-soluble salts of the compounds of formula I may be the alkali metal and ammonium salts or the salts of organic bases, for example, the mono-, di- and tri-ethanolamines, alkyl and arylamines, and guanidine.

In our copending Application No. 30063/71 (Serial No. 1,392,043) there is described and claimed a process for inhibiting the attack of a corrosive water system on metals with which it comes into contact which comprises incorporating in the system a phosphonic acid of the general formula:—

$$R^1\!\!-\!\!N\!\!\begin{array}{c} \diagup \; CH_2PO_3H_2 \\[1em] \diagdown \; CH_2PO_3H_2 \end{array}$$
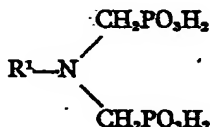
in which R^1 is a straight-chain alkyl group containing from 1 to 5 carbon atoms, an alkenyl group containing from 3 to 5 carbon atoms in which the double bond is not adjacent to the nitrogen atom, a tolyl group, a benzyl group or a cyclohexyl group or a water-soluble salt thereof.

In this specification, we define synergism in terms of the graphical interpretation of the results derived from a simple test for corrosion inhibition properties of materials. In this test, the effectiveness of an additive as a corrosion inhibitor in aqueous solution is measured in terms of the loss of metal from a test specimen immersed in the aqueous solution under standard conditions. A result is obtained to show the efficiency of inorganic nitrite by itself as a corrosion inhibitor, and a result is obtained to show the efficiency of the aminoalkyl phosphonic acid under test by itself as a corrosion inhibitor; these are plotted on a graph as the figures for 100% inorganic nitrite and 100% aminoalkyl phosphonic acid. Combination such as 80% nitrite/20% aminoalkyl phosphonic acid, 60% nitrite/40% aminoalkyl phosphonic acid, 40% nitrite/60% aminoalkyl phosphonic acid and 20% nitrite/80% aminoalkyl phosphonic acid are then tested until a clear graph can be plotted to show the effectiveness as a corrosion inhibitor of all combinations of the nitrite and aminoalkyl phosphonic acid under test. This graph is plotted, and at the same time the linear interpolation between the values for 100% inorganic nitrite and 100% aminoalkyl phosphonic acid is drawn. We define a combination of inorganic nitrite and aminoalkyl phosphonic acid as a synergistic combination if the value of corrosive weight loss observed in practice by means of this test is 90% of or less than 90% of the value of the corrosive weight loss for that combination on the linear interpolation between the values for 100% inorganic nitrite and 100% aminoalkyl phosphonic acid.

The test method we use will be referred to as the Aerated-Solution Bottle Test, and is described in detail as follows:

The apparatus itself is described with reference to the drawings accompanying the provisional specification.

Figure 1 is a longitudinal section of the bottle used for the test to show a length of glass tubing cemented to the inside of the bottle using "Araldite" resin AY103 in conjunction with hardener HY965 ("Araldite" is a Trade Mark). About 2 grams of the mixture for each bottle is usually required.

Figure 2 is a transverse cross-section of the bottle used for the test.

Figure 3 is a longitudinal section of the bottle in use during the test showing the connections and contents.

Figure 4 is a contracted longitudinal section of a water-distributor with T-pieces.

Figure 5 is a cross-section of a water distributor with a T-piece.

Figure 6 is a perspective view of the whole apparatus.

Referring to Figures 1 and 2, the bottle, 10, having a volume of approximately 130 millilitres has attached to the inside wall by means of cement, 11, a glass chimney, 12, which is two inches in length and positioned so that there is a ¼ inch gap between the bottom of the tube and the bottom of the bottle.

In Figure 3 the bottle, 10, is shown with a mild steel test coupon, 24, suspended from the neck of the bottle by a nylon thread, 25, which is held in position round the neck by a rubber band, 26. A piece of polythene tubing, 19, dips below the surface of the water, 27, in the bottle, 10, and another piece of polythene tubing, 28, having an internal diameter of 0.030 inches fitted with a jet, 29, passes into the glass chimney, 12, and terminates near the bottom of the glass chimney.

Referring to Figures 4 and 5, a distributor, 13, made from copper tubing 17 inches in length and having an outside diameter of ⅜ inch, is sealed at one end, 14. The other end, 15, is threaded to take a nozzle 16 and polythene tubing, of ¼ inch internal diameter is fitted over this nozzle. Into the copper tube are welded 30 pieces of copper tubing, 17, each of which are 2 inches long, have an internal diameter of 1/16 inch and are spaced ½ inch apart to form effectively 30 T-pieces.

In Figure 6, the bottles, 10, are placed in a thermostatted water-bath, 18. Pushed over the end of the T-pieces, 17, are lengths of polythene tubing, 19, approximately 12 to 15 inches in length and ½ inch internal diameter. A 2-litre water reservoir, 20, is connected to each of the bottles via the distributor, 13, and polythene tubing, 19, dipping below the surface of the liquid in each of the bottles, 10. The reservoir is tightly stoppered with a long glass tube, 21, passing through a rubber bung, 22, to the bottom of the reservoir. A small hole, 23, is made in the wall of the tube near the bottom.

In the test itself a sample of the mixture to be tested is added to a 100 millilitre sample of a synthetic corrosive water having the following composition

20   grams CaSO₄ . 2H₂O
15   grams MgSO₄ . 7H₂O
4.6   grams NaHCO₃
7.7   grams CaCl₂ . 6H₂O
45   gallons of distilled water.

The concentration of the mixture to be tested is 100 parts of mixture per million parts of synthetic corrosive water.

A mild steel test coupon (5 × 2.5 centimetres), which has been scrubbed with pumice, dipped for one minute in hydrochloric acid, dried and weighed, is suspended below the surface of the solution. The solution is then stored at 40°C in the thermostatted water bath.
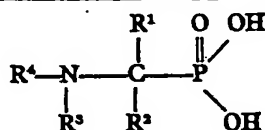
During the storage period the bottle is continuously aerated by passing air (500 millilitres/minute) through the tube, 28, screen from the metal surface by the glass chimney, 12. The aeration of the bottle is controlled by a rotameter calibrated in litres per minute which is connected to an air supply. The outlet of the rotameter is connected by polyethene tubing to a distributor constructed similarly to that already described. Control of the air bubble size and individual aeration rates in each bottle is achieved by using the polythene tubing, 28, with the jet, 29. Water losses caused by evaporation are replenished with deionised water dispensed from a constant head device, this being the 20-litre water reservoir which is connected to the distributor, 13 by polythene tubing and then to the bottle containing the sample by more polythene tubing. The position of the glass tube, 21, in the reservoir is adjusted so that the level of the hole, 23, coincides with the required water level in the bottle under test.

After 48 hours the mild steel coupon is removed, scrubbed with pumice, dipped in hydrochloric acid inhibited with 1% by weight of hexamine for one minute and re-weighed.

The corrosion rate is recorded as the weight loss in terms of milligrams per square decimetre per day (m.d.d.). Each test is carried out on duplicate specimens.

The following particular classes of compounds may be selected from the general formula I.
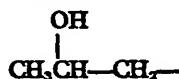
Class I having the formula:

$$R^4-N-\overset{\overset{\displaystyle R^1}{|}}{\underset{\underset{\displaystyle R^3}{|}}{C}}-\overset{\overset{\displaystyle R^2}{|}}{\underset{\underset{\displaystyle OH}{\diagup}}{\overset{\overset{\displaystyle O}{\|}}{P}}}\diagdown OH$$

II

derived from the general formula I where m=0, R^1, R^2, R^3 and R^4 represent hydrogen, hydrocarbyl or hydroxy substituted hydrocarbyl, R^3 and R^4 represent carboxyalkyl, or R^3 and R^4 together with the nitrogen atom may form a 6-membered ring, and the total number of carbon atoms in the groups R^3 and R^4 together does not exceed 10.
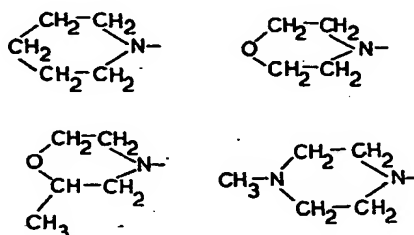
The hydrocarbyl or hydroxy substituted hydrocarbyl group may be:

a   alkyl, for example methyl, ethyl, n-propyl, isopropyl, n-butyl, sec-butyl, t-butyl, n-hexyl, n-octyl or t-octyl group but preferably a methyl group.

b   aryl, for example phenyl

c   alkaryl, for example o,m,p-tolyl

d   aralkyl, for example benzyl

e   alkenyl, for example allyl, α-methallyl, crotonyl

f   cycloalkyl, for example cyclohexyl

g   hydroxyalkyl, for example: $HO \cdot CH_2CH_2-$ $HO \cdot CH_2CH_2CH_2-$ or

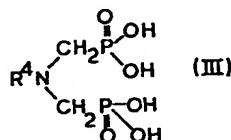$$\overset{\overset{\displaystyle OH}{|}}{CH_3CH-CH_2-}$$

The carboxyalkyl group may be for example carboxymethyl or β-carboxyethyl groups.

The six-membered ring may be for example:

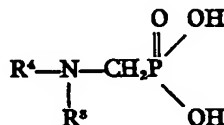Class II having the formula:

$$R^4N\overset{\diagup CH_2P\overset{\overset{\displaystyle O}{\|}}{\diagup}\overset{OH}{\diagdown OH}}{\diagdown CH_2P\overset{OH}{\diagdown OH}}$$

(III)

derived from the formula I where m=0, R^1 and R^2 are both hydrogen, and R^3 is a methylene phosphonic acid grouping. R^4 is a hydrocarbyl or hydroxy substituted hydrocarbyl radical.
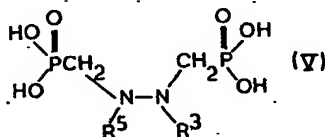
Class III having the formula:

$$R^4-N-\underset{\underset{\displaystyle R^3}{|}}{CH_2}\overset{\overset{\displaystyle O}{\|}}{P}\overset{\overset{\displaystyle OH}{\diagup}}{\diagdown OH}$$

IV

derived from formula I wherein m=0, and R^1 and R^2 are both hydrogen. R^3 is hydrogen or a methylene phosphonic acid grouping and R^4 is a hydroxy, —CH_2COOH or a —CH_2CH_2COOH grouping.

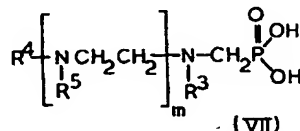Class IV having the formula:

derived from formula I wherein R^1 and R^2 are hydrogen, R^3 is hydrogen or a methylene phosphonic acid grouping, m=1, n=0, R^5 is hydrogen or a methylene phosphonic acid grouping and R^4 is a methylene phosphonic acid grouping.

Class V having the formula:
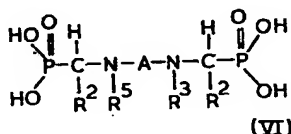
derived from the formula I where M=1, n=1, R^1 is hydrogen and R^4 is an alkylene phosphonic acid grouping. R^2 may be hydrogen or a hydroxy phenyl grouping, R^3 and R^5 are the same and are hydrogen or methylene phosphonic acid groupings and A is a saturated divalent hydrocarbyl, which may be linear or branched, containing from 1 to 6 carbon atoms and may be for instance a methylene, 1,2-ethylene, 1,3-propylene, 1,2-propylene, 1,4-butylene, 1,3-phenylene or 1,4-phenylene grouping; or the grouping R^3N—A—NR^5 may form a ring for instance to give a piperazinyl grouping.

Class VI having the general formula:

derived from formula I where m is a positive integer from 2 to 60, n=1 and A is a 1,2-ethylene grouping. R^3, R^4 and R^5 may each be hydrogen or a methylene phosphonic acid grouping, provided that at least 50% of these groups are methylene phosphonic acid groups, and that not all the R^5 groupings need be identical.
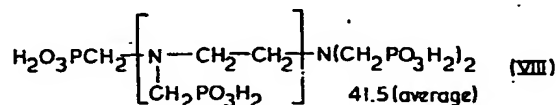
Examples of compounds of Class I are α-anilino ortho-hydroxy benzyl phosphonic acid, piperidino methylene phosphonic acid and amino methane phosphonic acid.

Examples of compounds of Class II are methyl amino di(methylene phosphonic acid), ethyl amino di(methylene phosphonic acid), n-pentylamino di(methylene phosphonic acid), n-hexylamino di(methylene phosphonic acid), p-toluidino di(methylene phosphonic acid), β-hydroxy ethyl amino di(methylene phosphonic acid), n-propylamino di(methylene phosphonic acid), allylamino di(methylene phosphonic acid) and cyclohexylamino di(methylene phosphonic acid).

An example of a compound of Class III is hydroxy amino methylene phosphonic acid or carboxy methyl amino di(methylene phosphonic acid) or hydroxy amino di(methylene phosphonic acid). An example of a compound of Class IV is hydrazine tetra(methylene phosphonic acid).

An example of a compound of Class V is ethylene diamine tetra(methylene phosphonic acid).

An example of a compound of Class VI is a compound having the formula:

$$H_2O_3PCH_2 \left[\begin{array}{c} N-CH_2-CH_2 \\ | \\ CH_2PO_3H_2 \end{array} \right] N(CH_2PO_3H_2)_2 \quad \text{(VIII)}$$
41.5 (average)

We have found that compositions of the present invention containing a compound of Class I, II, V or VI form synergistic combinations with from 10% to 95% by weight of sodium nitrite: compositions of the present invention containing a compound of Class III form synergistic combinations with from 10% to 90% by weight of sodium nitrite: and compositions of the present invention containing a compound of Class IV form synergistic combinations with from 10% to 80% by weight of sodium nitrite.

In order to illustrate the synergism obtained more clearly, Graphs 1 to 6 in the accompanying drawings were plotted to show the efficiency as corrosion inhibitors of mixtures of sodium nitrite and a compound of each of the classes 1 to 6. Graphs 1 to 6 show the variation of the corrosion ratio against the percentage of sodium nitrite in the mixture. The corrosion ratio is defined as the corrosion rate in the presence of the mixture divided by the corrosion rate in the presence of 100% sodium nitrite. The value for 100% sodium nitrite is, therefore, 1 in all examples.

In the graphs accompanying the provisional specification, graph 1 shows the synergism obtained for a mixture containing methylamino di(methylene phosphonic acid), a compound of Class II; Graph 2 shows the synergism obtained for a mixture containing hydrazine tetra(methylene phosphonic acid), a compound of Class IV; Graph 3 shows the synergism obtained for α-anilino o-hydroxy benzyl phosphonic acid, a compound of Class I. Graph 4 shows the synergism obtained for carboxy methylamino di(methylene phosphonic acid), a compound of Class III; Graph 5 shows the synergism obtained for ethylene diamine tetra(methylene phosphonic acid) a compound of Class V; and Graph 6 shows the synergism of a compound of Class VI wherein m has an average value of 41.5.

From these graphs, it can easily be seen that excellent results are obtained when the compounds of formula I present in the mixtures are hydrazine tetra(methylene phosphonic acid), ethylene diamine tetra(methylene phosphonic acid), methylamino di(methylene phosphonic acid) and α-anilino ortho hydroxy benzyl phosphonic acid.

Particularly preferred synergistic combinations of the present invention are those where the value of corrosion observed in practice by means of this test is 50% or less than 50% of the value of the corrosion for that combination on the linear interpolation between the values for 100% inorganic nitrite and 100% aminoalkylphosphonic acid. As can be seen from the graphs, mixtures which give such a corrosion value are:

1. Mixtures of methylaminodi(methylene phosphonic acid) and sodium nitrite consisting of from 30% to 85% sodium nitrite.
2. Mixtures of hydrazine tetra(methylene phosphonic acid) and sodium nitrite consisting of from 22% to 30% of sodium nitrite.
3. Mixtures of α-anilino ortho hydroxy benzyl phosphonic acid and sodium nitrite consisting of from 30% to 85% of sodium nitrite.
4. Mixtures of ethylene diamine tetra(methylene phosphonic acid) and sodium nitrite consisting of from 25% to 85% sodium nitrite.
   Mixtures of the compound of Class VI where the average value of m is 41.5 and sodium nitrite consisting of from 20% to 80% sodium nitrite.

The nitrite that is used may be an alkali metal nitrite, for example, potassium nitrite, but is preferably sodium nitrite.

The present invention also provides an aqueous system containing a synergistic combination as hereinbefore defined.

Furthermore there is provided a method of forming or replenishing an inhibited aqueous solution which comprises adding to the system inorganic nitrite or a compound of formula I or both such that the final inhibited aqueous solution contains both ingredients and in such quantities that the effect of their addition is to cause synergism as hereinbefore defined. Conveniently, the corrosion inhibiting mixture is present in an amount of from 50 to 10,000 parts per million of the aqueous solution. However amounts greater than 200 parts per million are usually unnecessary except when added in initial 'shock' doses.

If desired there may be added to the mixture, specific corrosion inhibitors for non-ferrous metals such as a silicate to control attack on aluminium, or a specific inhibitor to control attack on (or induced by) copper. There may also be added other

1,392,044

corrosion inhibitors for ferrous metals known per se, e.g. zinc ions, polyphosphate or chromium ions or amines.

The following Examples further illustrate the present invention. Parts and percentages are expressed by weight.

Examples 1 to 8.

In each of the following Examples, four mixtures were made up from sodium nitrite and a compound of formula I as illustrated in Table 1, each mixture containing 20%, 40%, 60% and 80% by weight of the compound of formula I respectively. Samples of each of these mixtures were added to 100 millilitre samples of the aggressive as hereinbefore defined water so that four solutions were prepared each containing 100 parts per million of the mixture. The aerated bottle test was carried out on these solutions.

In order to demonstrate the synergistic effect of the mixtures of the present invention when compared with the individual constituents of the mixture, samples containing sodium nitrite and the respective compound of formula I were tested separately in a similar manner at concentrations of 100 parts per million. The corrosion ratio was calculated as hereinbefore defined and the results are shown in Table 1.

The results obtained clearly show the synergism of mixtures of the present invention.

Examples 9 to 20.

The same procedure described in Examples 1 to 8 was followed except that instead of four mixtures, three mixtures were made up containing 25%, 50% and 75% by weight of various other compounds of formula I. The results are shown in Table 2.

Examples 21 and 22.

The same procedure described in Examples 1 to 8 was followed except that instead of four mixtures, three mixtures were made up containing 25%, 50% and 75% by weight of various other compounds of formula I. The results are shown in Table 3.

TABLE 3

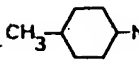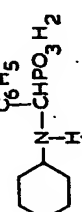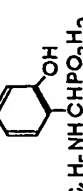| Formula	100%	75%	50%	25%	0%
$\text{—N (CH}_2\text{PO}_3\text{H}_2)_2$, CH$_3$ CH$_3$	1.3	0.24	0.18	0.27	1.00
$CH_3\text{—}\text{—N (CH}_2\text{PO}_3\text{H}_2)_2$	0.75	0.15	0.14	0.12	1.00

TABLE 1

Example	Compound of Formula 1	Corrosion Ratio of mixtures containing varying percentages of compound of formula 1					
		100%	80%	60%	40%	20%	0%
1	$CH_3N(CH_2PO_3H_2)_2$	0.88	0.59	0.16	0.08	0.19	1.00
2	$C_2H_6N(CH_2PO_3H_2)_2$	1.19	0.69	0.51	0.14	0.33	1.00
3	$CH_3(CH_2)_2N(CH_2PO_3H_2)_2$	1.79	1.09	0.25	0.42	0.39	1.00
4	$CH_2{=}CHCH_2N(CH_2PO_3H_2)_2$	0.37	0.15	0.05	0.31	0.24	1.00
5	$nC_6H_{13}N(CH_2PO_3H_2)_2$	2.25	0.96	0.37	0.01	0.20	1.00
6	CH_3—C₆H₄—$N(CH_2PO_3H_2)_2$	1.28	0.95	0.81	0.33	0.47	1.00
7	cyclohexyl—$N(C_6H_5)$—$CHPO_3H_2$	1.20	0.89	0.72	0.06	0.68	1.00
8	$C_6H_5NHCHPO_3H_2$ (with OH-substituted phenyl)	1.08	0.56	0.09	0.02	0.78	1.00

TABLE 2

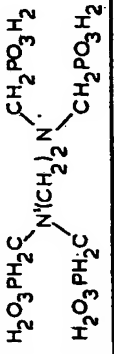| Example	Compound of Formula I	Corrosion Ratio of Mixtures Containing varying Percentages of Compound of Formula I				
		100%	75%	50%	25%	0%
9	$CH_3(CH_2)_3N(CH_2PO_3H_2)_2$	0.63	0.36	0.34	0.62	1.00
10	$nC_6H_{11}N(CH_2PO_3H_2)_2$	1.04	0.32	0.57	0.88	1.00
11	$\bigcirc\!-\!N(CH_2PO_3H_2)_2$	0.41	0.33	0.04	0.33	1.00
12	$HOCH_2CH_2N(CH_2PO_3H_2)_2$	0.62	0.44	0.55	0.55	1.00
13	$HOOCCH_2N(CH_2PO_3H_2)_2$	0.73	0.61	0.52	0.80	1.00
14	$H_2NCH_2PO_3H_2$	0.87	0.36	0.54	0.54	1.00
15	$H_2O_3PH_2C \backslash N(CH_2)_2 N / {}^{CH_2PO_3H_2}_{CH_2PO_3H_2}$ with $H_2O_3PH_2C$	0.62	0.28	0.06	0.03	1.00
16	(cyclohexane ring)$-NCH_2PO_3H_2$	0.21	0.24	0.45	0.49	1.00

TABLE 2 (Continued)

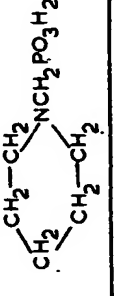| Example	Compound of Formula I	Corrosion Ratio of Mixtures Containing varying Percentages of Compound of Formula I				
		100%	75%	50%	25%	0%
17	$H_2O_3PCH_2 - N \left[\begin{array}{c} CH_2PO_3H_2 \\ - CH_2 - CH_2 - \end{array} \right]_4 N(CH_2PO_3H_2)_2$	0.48	0.55	0.51	0.80	1.00
18	$H_2O_3PCH_2 - N \left[\begin{array}{c} CH_2PO_3H_2 \\ - CH_2 - CH_2 - \end{array} \right]_{13.5 \text{ (average)}} N(CH_2PO_3H_2)_2$	0.09	0.07	0.08	0.48	1.00
19	$H_2O_3PCH_2 - N \left[\begin{array}{c} CH_2PO_3H_2 \\ - CH_2 - CH_2 - \end{array} \right]_{41.5 \text{ (average)}} N(CH_2PO_3H_2)_2$	0.11	0.13	0.17	0.27	1.00
20	$\begin{array}{c} H_2O_3PH_2C \\ H_2O_3PH_2C \end{array} N - N \begin{array}{c} CH_2PO_3H_2 \\ CH_2PO_3H_2 \end{array}$	1.07	0.44	0.74	0.86	1.00

Some further laboratory tests were carried out using a Laboratory Heat Exchanger Rig, a form of laboratory testing intended to simulate practical use conditions more closely than does the Aerated Solution Bottle Test just described. In this rig, corrosive water is aerated and circulated over a number of metal coupons, and is heated by being passed through a heated steel heat exchanger tube. After a suitable test period, the metal coupons and the heat exchanger tube are examined, and their state assessed.

In detail, the rig consists of a closed water circuit, made up of the following items in order,

                    2 litre reservoir
                    1 litre reservoir
                    flow meter
                    coupon chamber
                    heat exchanger
                    cooling condenser

Corrosive water in the 2 litre reservoir is aerated with compressed air introduced through a sintered disc at about 5 litres per minute, and is then pumped to the 1 litre reservoir. From this reservoir it is pumped through the flow meter to the glass coupon chamber in which are a number of rectangular metal coupons each 2.5 by 5.0 cms. mounted on a perspex jig ("Perspex" is a Trade Mark). The water then flows through the heat exchanger which is made up of a ⅝ inch internal diameter steel tube with copper end pieces around which is wound a 960 watt heater coil; from the heat exchanger the water flows through the cooling condenser back to the 2 litre reservoir.

A flow rate in the circuit of about 1.0 gallon per minute provides a velocity of about 1.5 feet per second and a Reynolds number of 8500 in the heat exchanger. The heater coil gives the heat exchanger tube a skin temperature of about 60°C. and the water leaves at about 45°C., a difference across the heat transfer surface of some 15°C. The cooling condenser is so operated as to cool the water to about 35°C. before it begins a fresh circuit.

Metal coupons are scrubbed with pumice and then immersed in acid as follows:

metal	acid
mild steel	Conc. HCl diluted 1:1 with water at room temperature for 1 minute
copper	” ”
brass	” ”
aluminium	5% phosphoric acid/2% chromic acid, at 75°C. for 5 minutes

After such immersion, the coupons are rinsed with water, dried and weighed; they are then mounted on a perspex jig, care being taken to ensure that none of the coupons touch each other, and that they are insulated from the bolt holding the jig together. The mild steel heat exchanger is cleaned with pumice, dipped in conc. hydrochloric acid diluted 1:1 with water, and then rinsed in water and dried.

The rig is assembled using a glass tube in place of the heat exchanger by circulating conc. hydrochloric acid diluted 1:1 with water, then flushing with tap water for about half an hour (about 30 gallons in all) and draining. The freshly cleaned specimens are then placed in the coupon chamber and the heat exchanger is mounted in position. The necessary quantity of additives to produce the desired concentrations is put into one of the reservoirs and the rig is filled with 4.5 litres of a standardised corrosive test water, which is characterised as follows:—

Phenol Alkalinity	: 0	
Total Alkalinity	: 20	as p.p.m of CaCO₃
Total Hardness	: 80	
Chloride	: 10	p.p.m.
Conductance	: 180	mhos

The pump is primed and started and the heater switched on.

The concentration of inhibitor an dthe water level in the rig are checked daily and any losses made good.

After a standard period of ten days, the heat exchanger tube is removed, sectioned and examined; the test coupons are removed, cleaned as before except that the acid is in each case inhibited with 1% hexamethylene tetramine, rinsed, dried and re-weighed. The results observed enable an assessment to be made of the anti-scaling and anti-corrosive action of the inhibitor under test.

The following additives were tested, all parts and percentages being by weight:—

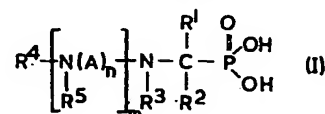| Run	Additives and Concentrations
1	None
2	200 ppm Sodium nitrite
3	200 ppm { 20% methylamino dimethylene diphosphonic acid / 80% sodium nitrite
4	400 ppm { 20% methylamino dimethylene disphosphonic acid / 80% sodium nitrite
5	100 ppm Zinc/Polyphosphate; 10.7% ZnO; 57% P_2O_5; 32.3% Na_2O

The results are illustrated in Table 4 and show quite clearly that synergistic mixtures of the present invention are better than corrosion inhibiting mixtures containing zinc ions.

TABLE 4

Run	CORROSION RATE OF METAL COUPONS mg. per sq. decimetre per day				Condition of Heat Exchange Tube
	Mild Steel	Copper	Brass	Aluminium	
1	69	42	15.6	5.5	SEVERELY CORRODED
2	42.5	1	5	25	WHOLE SURFACE ENCRUSTED WITH HEAVY CORROSION PRODUCTS
3	4.4	0.3	0.5	2.6	SMALL PATCHES OF CORROSION. REST OF TUBE SURFACE COVERED BY A PROTECTIVE GREEN FILM
4	1.8	1.6	1.0	1.3	"
5	19.4	0.8	2.4	2.7	CORROSION UNDER SCALE DEPOSIT

WHAT WE CLAIM IS:—

1. A synergistic combination (as hereinbefore defined) comprising a combination of an inorganic nitrite and a compound having the formula:
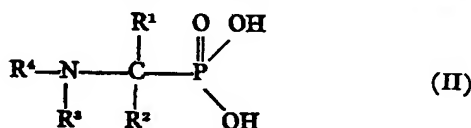
$$R^4 \left[N(A)_n \atop R^5 \right]_m N - \underset{R^3}{\overset{R^1}{\underset{|}{\overset{|}{C}}}} - \underset{R^2}{\overset{O}{\underset{|}{\overset{\parallel}{P}}}} \overset{OH}{\underset{OH}{}} \quad (I)$$

wherein R^1 and R^2 may be the same or different and each represents hydrogen or a or a hydrocarbyl or hydroxy-substituted hydrocarbyl radical each containing up to 8 carbon atoms, R^3 and R^4 may be the same or different and each represents hydrogen or a hydrocarbyl or hydroxy-substituted hydrocarbyl radical each containing up to 8 carbon atoms, a carboxyalkyl or alkoxyalkyl radical each containing up to 3 carbon atoms, an alkylene phosphonic acid grouping containing up to 4 carbon atoms or an aralkylene phosphonic acid such that not more than two phosphonic acid groupings separated by less than two carbon atoms may be attached to any nitrogen atom, R^5 is hydrogen or an alkylene phosphonic acid containing up to 4 carbon atoms, A is a saturated divalent hydrocarbyl radical containing up to 6 carbon atoms, m is 0 or an integer from 1 to 60, n is 0 or 1; when m is 0, R^4 may be a hydroxy grouping or R^3 and R^4 together with the nitrogen atom may form a six membered ring; when m is 1, the grouping R^5N—A—NR^5 may form a heterocyclic ring, and when m is greater than 1, the constituent R^5 groupings may be the same or different; and the water-soluble salts thereof.

2. A synergistic combination as claimed in Claim 1 in which the water-soluble salt of the compound of formula I is the alkali metal or ammonium salt.

3. A synergistic combination as claimed in Claim 1 in which the water-soluble salt of the compound of formula I is a mono-ethanolamine, di-ethanolamine, tri-ethanolamine, alkylamine, arylamine or guanidine salt.
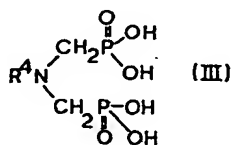
4. A synergistic combination as claimed in any of Claims 1 to 3 in which a particular class of compound selected from formula I has the general formula:

$$R^4 - \underset{R^3}{\overset{R^1}{\underset{|}{\overset{|}{N}}}} - \underset{R^2}{\overset{}{\underset{|}{C}}} - \underset{OH}{\overset{O}{\underset{}{\overset{\parallel}{P}}}} \overset{OH}{} \quad (II)$$

where R^1, R^2, R^3 and R^4 represent hydrogen, hydrocarbyl or hydroxy substituted hydrocarbyl, R^3 and R^4 represent carboxyalkyl, or R^3 and R^4 together with the nitrogen atom may form a 6-membered ring, and the total number of carbon atoms in the groups R^3 and R^4 together does not exceed 10.

5. A synergistic combination as claimed in Claim 4 in which the compound of formula II is α-anilino ortho-hydroxy benzyl phosphonic acid, piperidino methylene phosphonic acid or amino methane phosphonic acid.

6. A synergistic combination as claimed in any of Claims 1 to 3 in which a particular class of compound selected from formula I has the general formula:

$$R^4N \underset{CH_2P-OH}{\overset{CH_2P}{\underset{\parallel O}{}}} \overset{O}{\overset{\parallel}{\underset{OH}{P}}} \overset{OH}{} \quad (III)$$

where R^1 and R^2 are both hydrogen, R^3 is a methylene phosphonic acid grouping and R^4 s a hydrocarbyl or hydroxy substituted hydrocarbyl radical.

7. A synergistic combination as claimed in Claim 6 in which the compound of formula III is methyl amino di(methylene phosphonic acid), ethyl amino di(methylene phosphonic acid), n-hexylamino di(methylene phosphonic acid), p-toluidino di(methylene phosphonic acid) or β-hydroxy ethyl amino di(methylene phosphonic acid), n-pentylamino di(methylene phosphonic acid), n-propylamino di(methylene phosphonic

acid), allylamino di(methylene phosphonic acid), or cyclohexylamino di(methylene phosphonic acid).

8. A synergistic combination as claimed in any of Claims 1 to 3 in which a particular class of compound selected from formula I has the general formula:
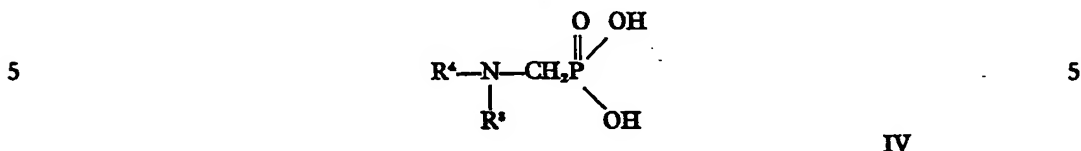

IV

wherein R^3 is hydrogen or a methylene phosphonic acid grouping and R^4 is a hydroxy, —CH_2COOH or a —CH_2CH_2COOH grouping.

9. A synergistic combination as claimed in Claim 8 in which the compound of formula IV is a hydroxy amino methylene phosphonic acid, carboxymethylamino di(methylene phosphonic acid) or hydroxy amino di(methylene phosphonic acid).
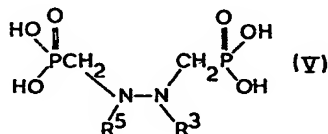
10. A synergistic combination as claimed in any of Claims 1 to 3 in which a particular class of compound selected from formula I has the general formula:

(V)

wherein each of the groupings R^3 and R^5 is hydrogen or a methylene phosphonic acid grouping.

1. A synergistic combination as claimed in Claim 10 in which the compound of formula V is hydrazine tetra(methylene phosphonic acid).

12. A synergistic combination as claimed in any of Claims 1 to 3 in which a particular class of compound selected from formula I has the general formula:

(VI)
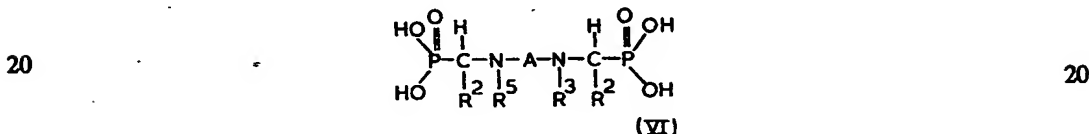
where R^2 is hydrogen or a hydroxy phenyl grouping, R^3 and R^5 are the same and are hydrogen or methylene phosphonic acid groupings and A is a linear or branched saturated divalent hydrocarbyl, containing from 1 to 6 carbon atoms; or the grouping R^3N—A—NR^5 may form a ring.

13. A synergistic combination as claimed in Claim 12 wherein A, in the compound of formula VI, is a methylene, 1,2-ethylene, 1,3-propylene, 1,4-butylene, m-phenylene or p-phenylene grouping.

14. A synergistic combination as claimed in Claim 12 or Claim 13 wherein the compound of formula VI is ethylene diamine tetra(methylene phosphonic acid).

15. A synergistic combination as claimed in any of Claims 1 to 3 in which a particular class of compound selected from formula I has the general formula:
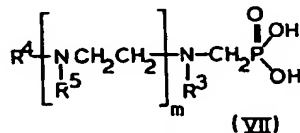

(VII)

where m is a positive integer from 2 to 60, R^3, R^4 and R^5 may each be hydrogen or a methylene phosphonic acid grouping, provided that at least 50% of these groups aer methylene phosphonic acid groups, and that not all the R^5 groupings need be identical.

16. A synergistic combination as claimed in Claim 15 in which the compound of formula VII is:

$$H_2O_3PCH_2 \left[\begin{array}{c} N-CH_2-CH_2 \\ \mid \\ CH_2PO_3H_2 \end{array} \right] N(CH_2PO_3H_2)_2 \quad (VIII)$$

41.5 (average)
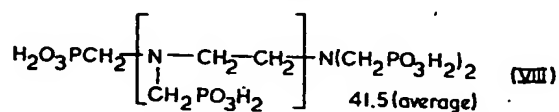
17. A synergistic combination as claimed in any of the preceding Claims in which the inorganic nitrite is sodium nitrite.

18. A synergistic combination as claimed in Claim 1 comprising a mixture consisting of methylamino di(methylene phosphonic acid) and from 30 to 85% by weight of sodium nitrite.

19. A synergistic combination as claimed in Claim 1 comprising a mixture consisting of hydrazine tetra(methylene phosphonic acid) and from 22% to 30% by weight of sodium nitrite.

20. A synergistic combination as claimed in Claim 1 comprising a mixture consisting of α-anilino ortho hydroxy benzyl phosphonic acid and from 30% to 85% of sodium nitrite.

21. A synergistic combination as claimed in Claim 1 comprising a mixture consisting of ethylene diamine tetra(methylene phosphonic acid) and from 25% to 85% sodium nitrite.

22. A synergistic combination as claimed in Claim 1 comprising a mixture consisting of a compound of formula VIII and from 20% to 80% sodium nitrite.

23. A synergistic combination as claimed in Claim 1 substantially as described in any of Examples 1 to 20.

24. An aqueous system containing from 50 to 200 parts per million of a synergistic combination as claimed in any of the preceding Claims.

25. A method of forming an inhibited aqueous solution which comprises adding to the system a synergistic combination of an inorganic nitrite and a compound of formula I as claimed in any of Claims 1 to 23.

26. A method of replenishing an inhibited aqueous system, as made by the method of claim 25, which comprises adding to the system an inorganic nitrite or a compound of formula I or both in such quantities that the effect of their addition is to cause synergism as hereinbefore defined.

27. A method of forming an inhibited aqueous solution in accordance with Claim 25 substantially as described in any of Examples 1 to 20.

28. A synergistic combination as claimed in Claim 1 substantially as described in Example 21 or 22.

29. A method of forming an inhibited aqueous solution in accordance with Claim 25 substantially as described in Example 21 or 22.

FIG.5.—

FIG.3.—

FIG.2.—

FIG.4.—

FIG.1.—

1392044 PROVISIONAL SPECIFICATION
5 SHEETS This drawing is a reproduction of
the Original on a reduced scale
Sheet 2

—FIG.6.—

—GRAPH 2—

—GRAPH 1—

CARBOXY METHYLAMINO DIMETHYLENE
DIPHOSPHONIC ACID

CORROSION RATIO

% SODIUM NITRITE

...—GRAPH. 4.—

∝—ANILINO ORTHO HYDROXY BENZYL PHOSPHONIC
ACID

% SODIUM NITRITE

—GRAPH.3.—

1392044   PROVISIONAL SPECIFICATION

5 SHEETS   *This drawing is a reproduction of*
the Original on a reduced scale
Sheet 5

$$\left[H_2O_3PCH_2\right]_N \begin{array}{c}CH_2PO_3H_2 \\ | \\ N \end{array} CH_2 \longrightarrow CH_2 \longrightarrow N \left(CH_2PO_3H_2\right)_2$$ 41.5

CORROSION RATIO

% SODIUM NITRITE

----GRAPH.6----

ETHYLENE DIAMINE TETRAMETHYLENE
TETRAPHOSPHONIC ACID

% SODIUM NITRITE

----GRAPH. 5----